

Intrinsically Elastic Actuation: A Novel Paradigm for High-Performance Torque Controlled Robots

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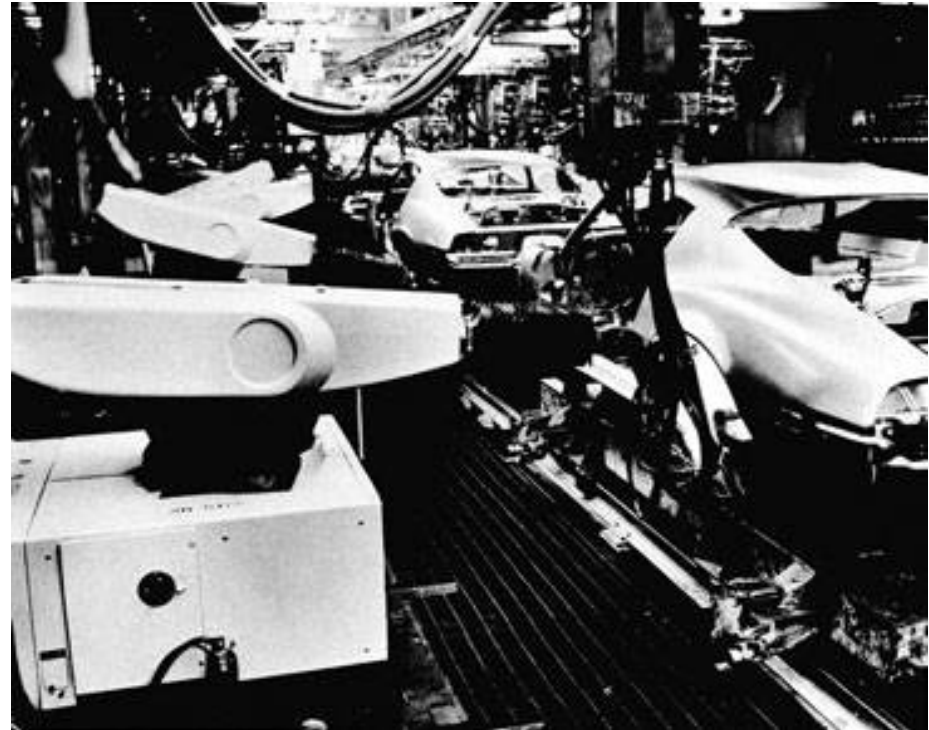
Robotics and Mechatronics Center
German Aerospace Center



Knowledge for Tomorrow



Unimate (Unimation)



- First industrial robot in first robot company (Unimation)
- Developed by George Devol and Joseph Engelberger in the 1950s using his original patent filed in 1954 and granted in 1961



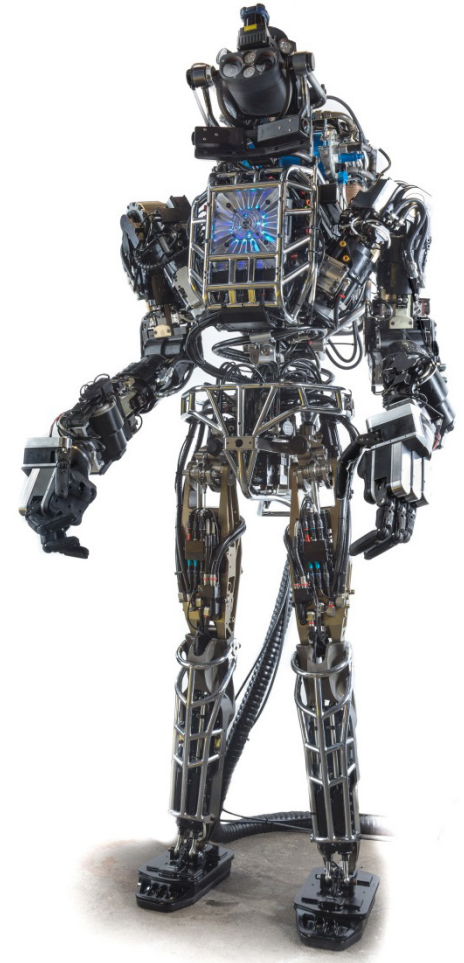
Humanoids



DLR, Germany



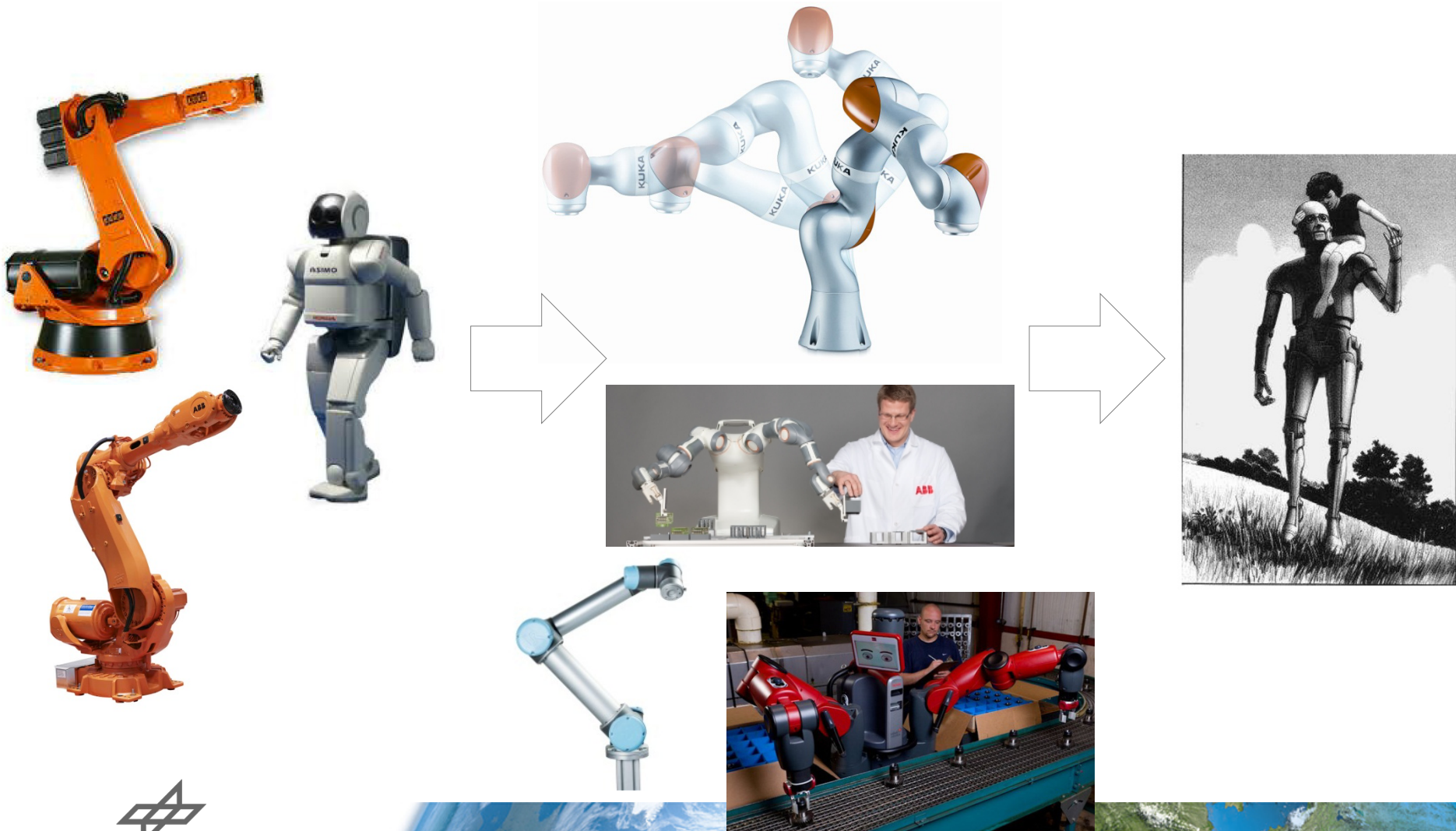
AIST, Japan



DARPA, USA



Paradigm Shift: New Generation of Robots



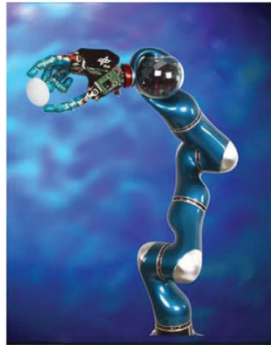
Enabler Technologies for Interaction: Lightweight Robots



LWR I (1992)



LWR II real (1999)



LWR III real (2002)



KINEMEDIC (2005)



Hand I (1998)



Hand II (2001)



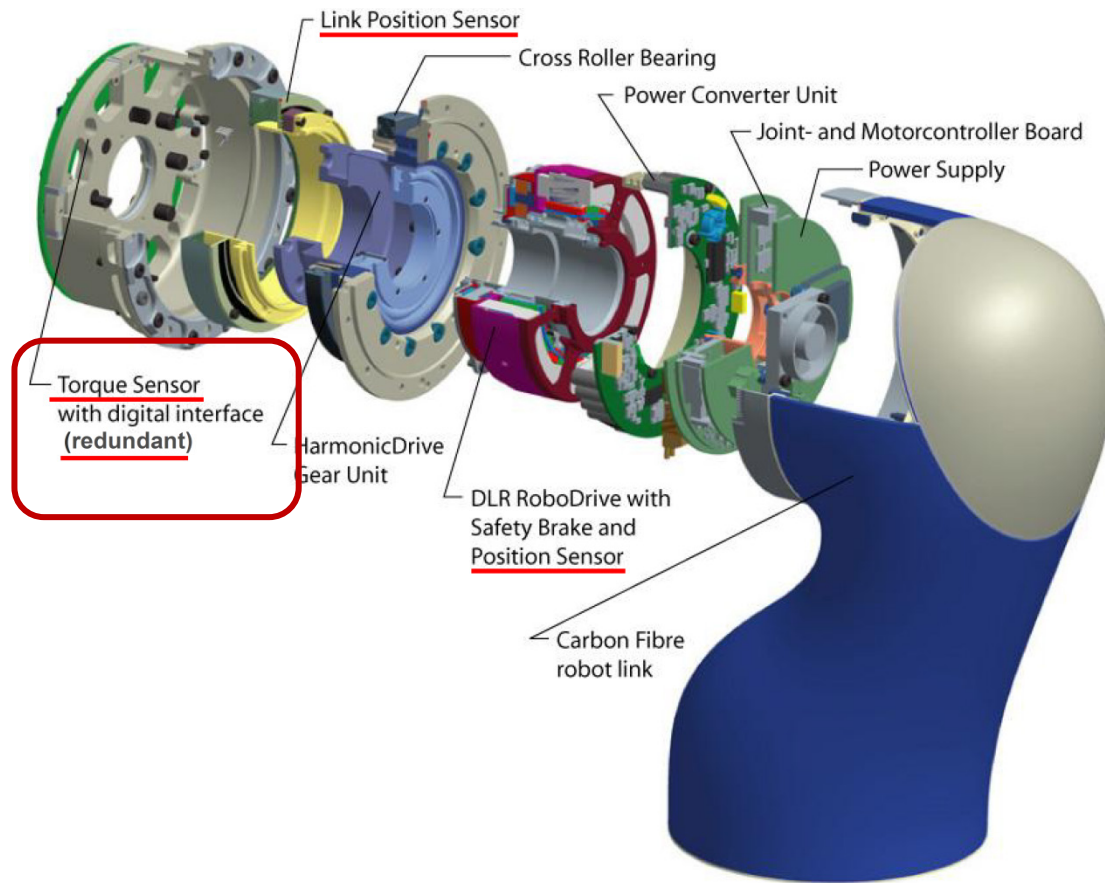
DLR's Lightweight Robots



Barrett's WAM Arm

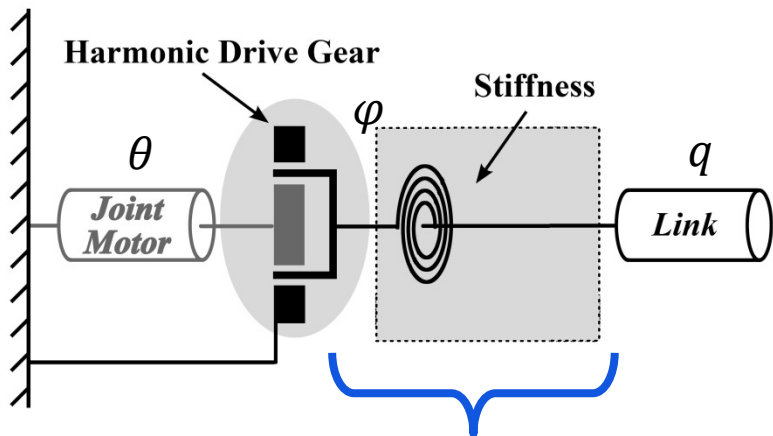


The Mechatronic Joint Design



Flexible joints

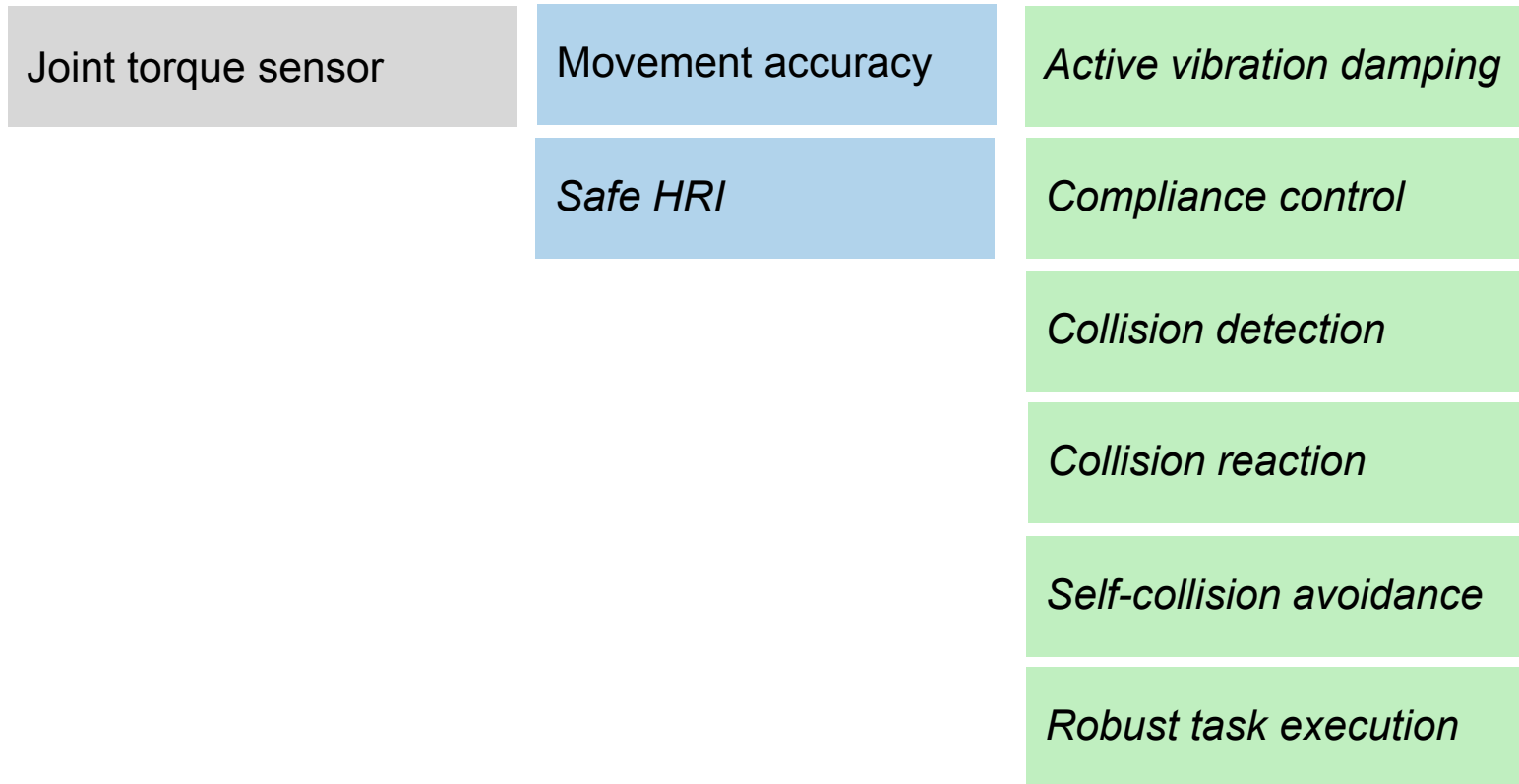
Joint model:



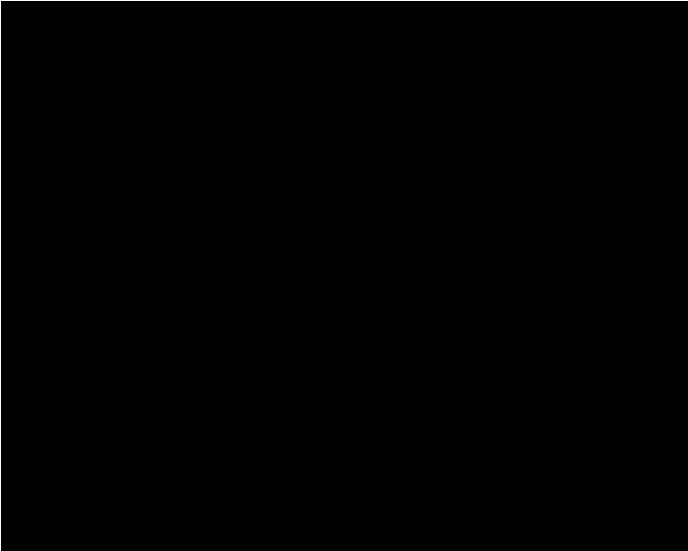
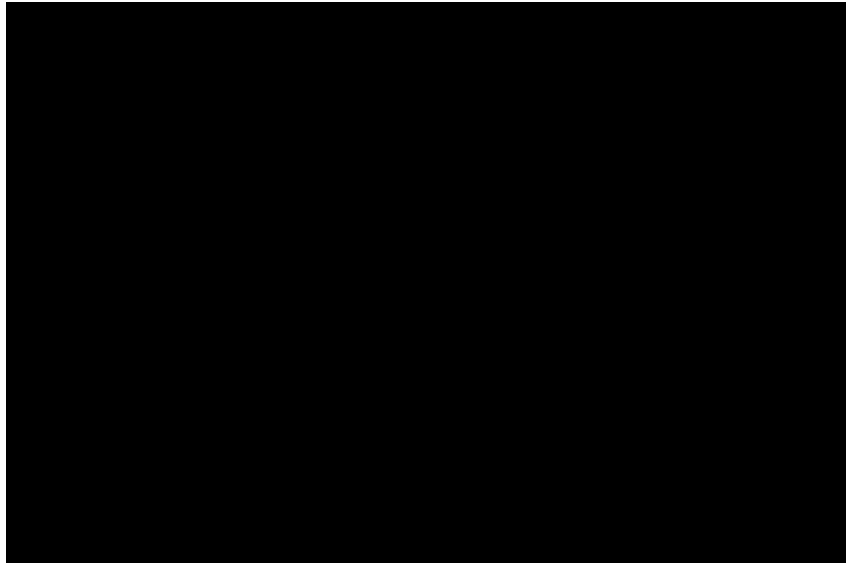
Strain gauge based torque sensor



Key Enabler: Joint Torque Sensor



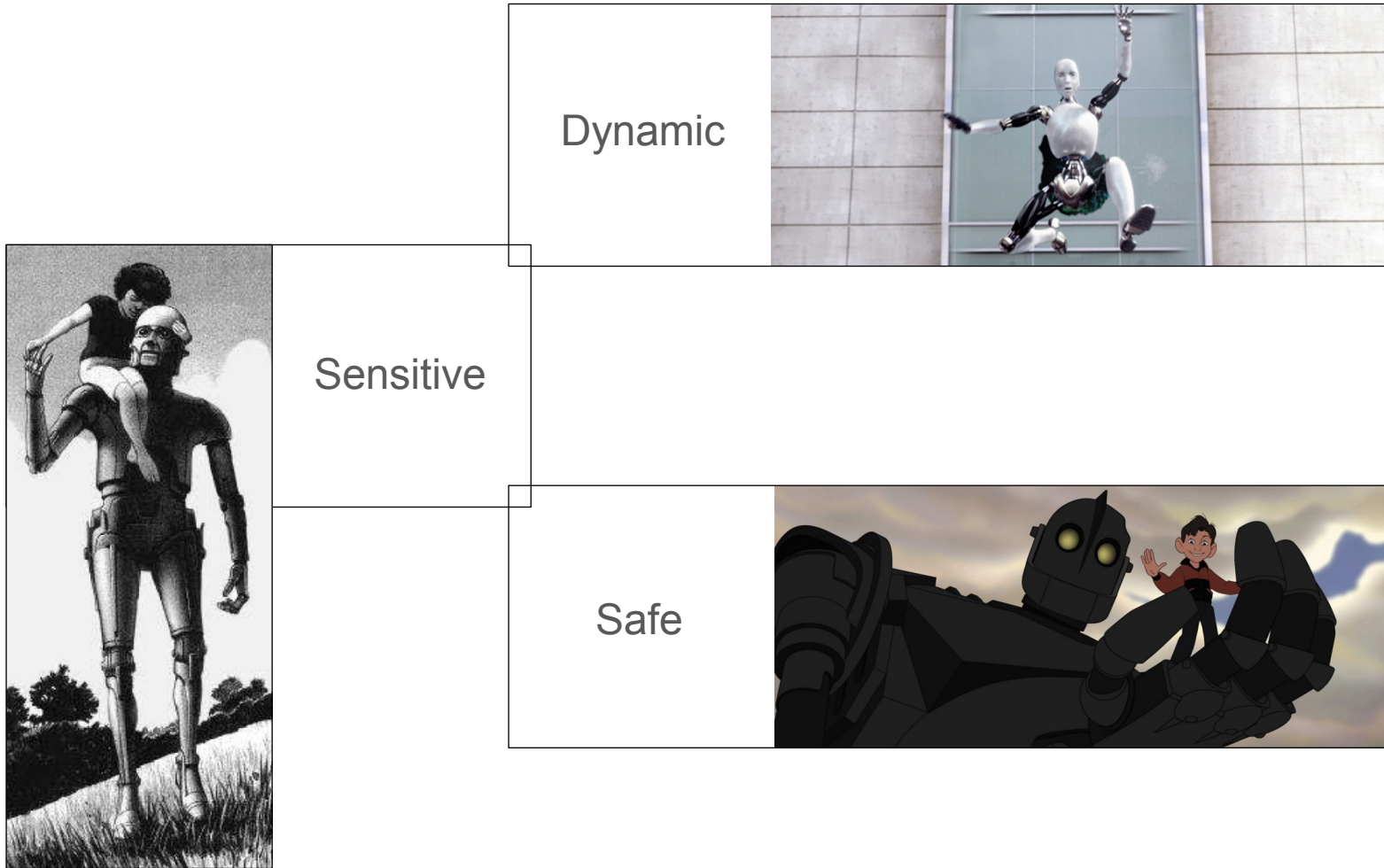
Possibilities



Performance Limitations of Rigid Robots



The Optimal Robot



Newest Robot Generation

rigid and heavy



passively compliant & light

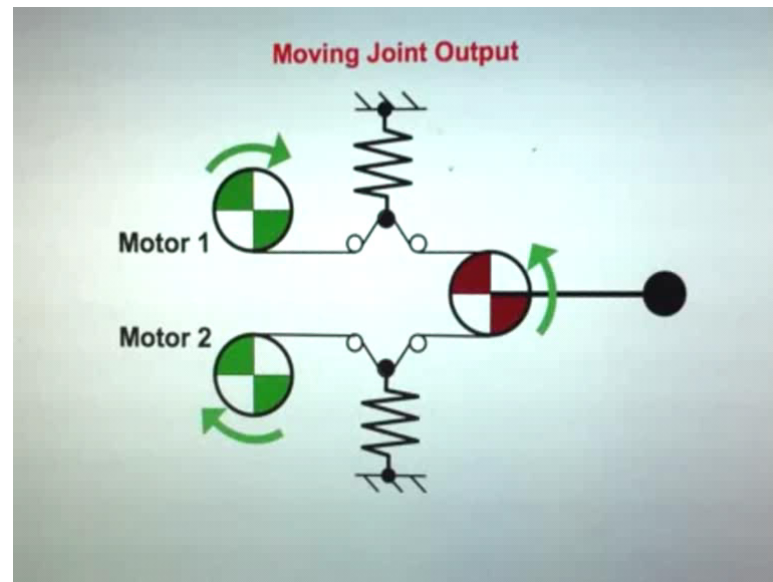
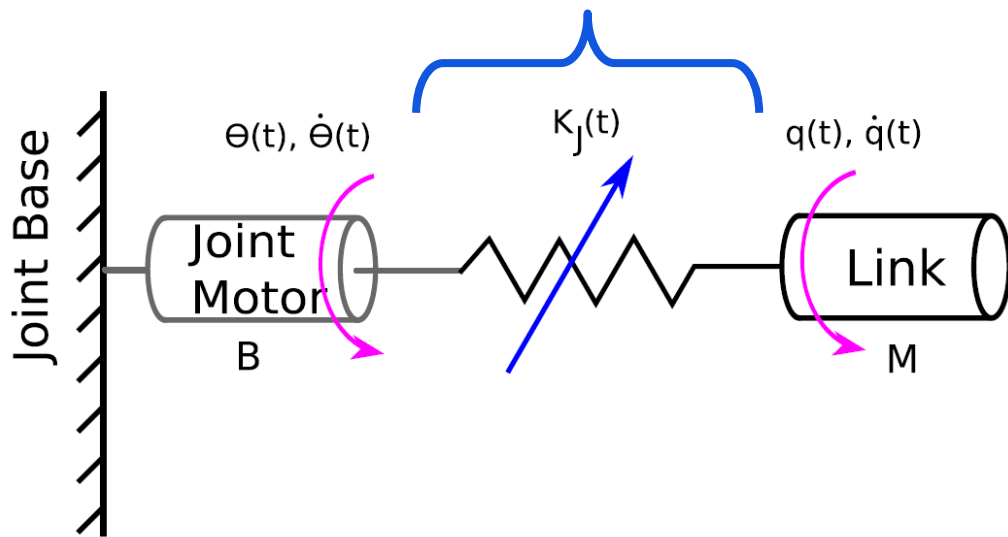


actively compliant & light

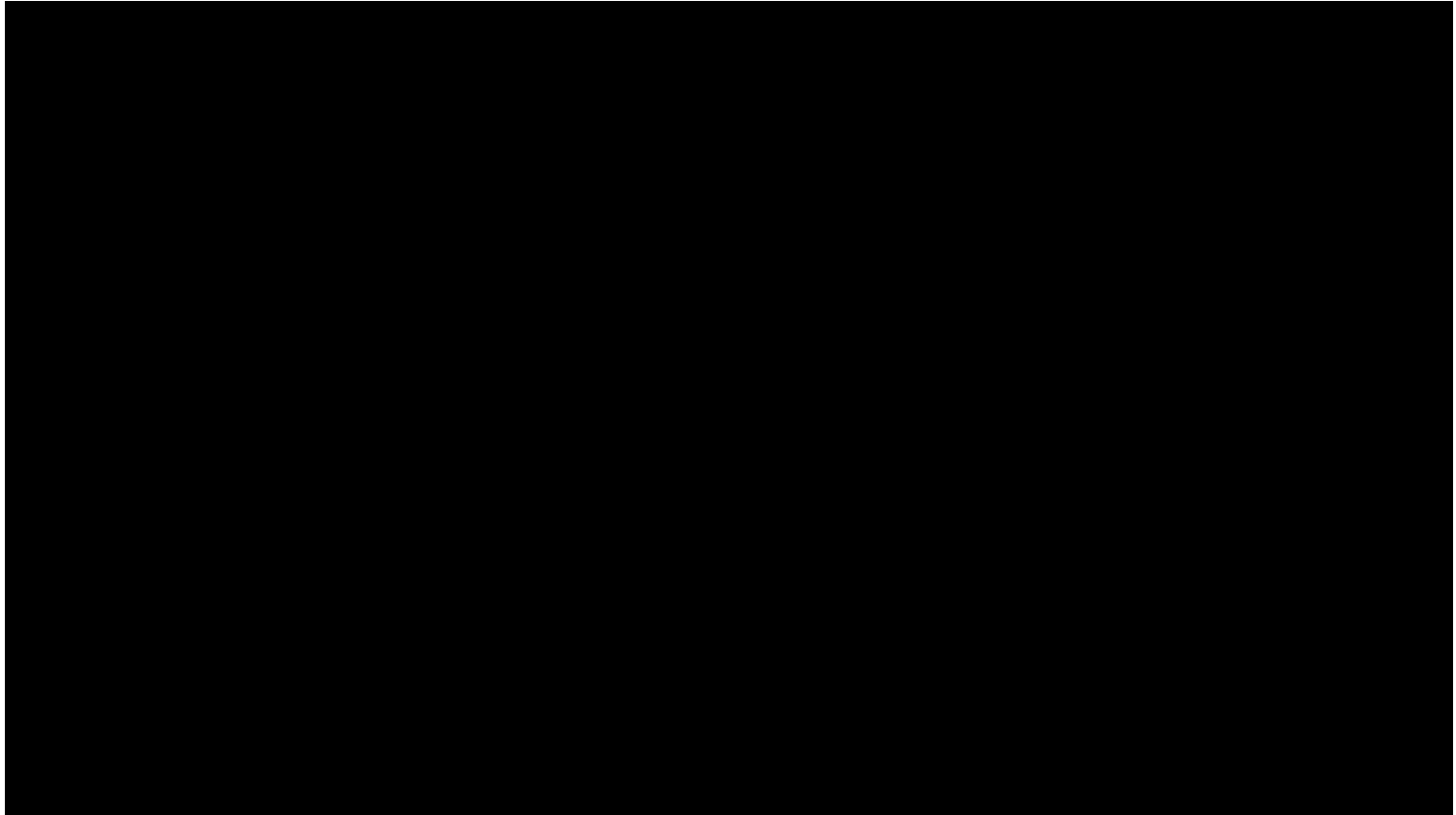


Elastic Robot Design

Torque Sensor implemented with two position sensors!



DLR Hand-Arm System



Problem Statement

Robots capable of high-performance safe interaction

AND

are able to achieve human like performance at the same time?



It is possible to store energy!



Can we transform this into kinetic energy?

In principle one should be able to move with the link considerably faster than maximum motor velocity!!



Exploiting Joint Elasticity



Key capabilities

- Elastic Joints:
 - Robustness
 - Performance
- Performance:
 - Maximize System Energy
 - Minimize Link Velocity
 - Time-Optimal Tracking
 - etc.



Optimal Control(OC) Problems



Pontryagin's Minimum Principle

$$\mathbb{H}(\mathbf{x}^*, \boldsymbol{\lambda}^*, u^*) \leq \mathbb{H}(\mathbf{x}^*, \boldsymbol{\lambda}^*, u)$$



Description with Physical Quantities



Optimal Control

- First-Order Differential Equations:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}, t)$$

- Inequality and End Constraints:

$$\mathbf{h}(\mathbf{x}(t), \mathbf{u}(t), t) \leq \mathbf{0} \quad \mathbf{g}(\mathbf{x}(t_f), t_f) = \mathbf{0}$$

and

- Cost Functional: $J(\mathbf{u}) = \underbrace{\vartheta(\mathbf{x}(t_f), t_f)}_{\text{Terminal Cost}} + \underbrace{\int_{t_0}^{t_f} L(\xi, \mathbf{x}(t), \mathbf{u}(t)) dt}_{\text{Running Cost}}$

$$J(\mathbf{u}^*) = \min_{\mathbf{u} \in \mathbb{U}} J(\mathbf{u})$$

Problem: Find the piecewise continuous Control: $\mathbf{u}^* \in \mathbb{U}$



Pontryagin's Minimum Principle (Unconstr. System)

- Hamiltonian:

$$\mathbb{H} = L(t, \mathbf{x}, \mathbf{u}) + \boldsymbol{\lambda}^T \mathbf{f}(t, \mathbf{x}, \mathbf{u})$$

- System Dynamics:

$$\dot{\mathbf{x}}^* = \left. \frac{\partial \mathbb{H}}{\partial \boldsymbol{\lambda}} \right|^* = \mathbf{f}((t, \mathbf{x}^*, \mathbf{u}^*)), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

- Costates Dynamics:

$$\dot{\boldsymbol{\lambda}}^* = - \left. \frac{\partial \mathbb{H}}{\partial \mathbf{x}} \right|^*, \quad \boldsymbol{\lambda}^*(t_f) = \frac{\partial \vartheta}{\partial \mathbf{x}}(\mathbf{x}(t_f), t_f)$$

- Minimum Principle:

$$\mathbb{H}(t, \mathbf{x}^*, \boldsymbol{\lambda}^*, \mathbf{u}^*) \leq \mathbb{H}(t, \mathbf{x}^*, \boldsymbol{\lambda}^*, \mathbf{u}), \quad \forall \mathbf{u} \in \mathbb{U}$$



Considered Problems

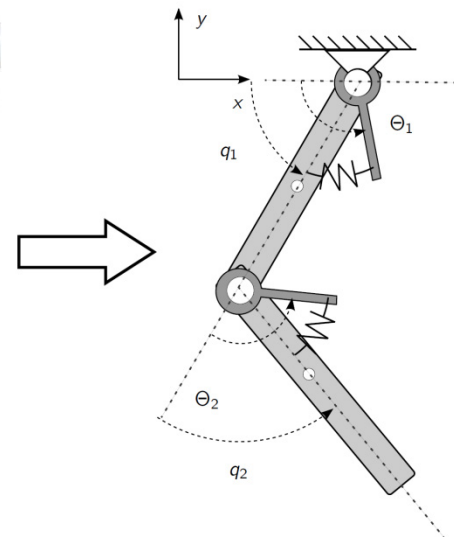
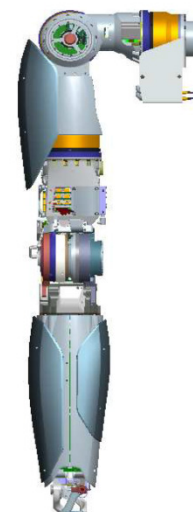
Focus: Problems with no Running Costs

$$J(u) = \vartheta(\boldsymbol{x}(t_f), t_f) \longrightarrow \text{Fully Exploiting System Dynamics}$$

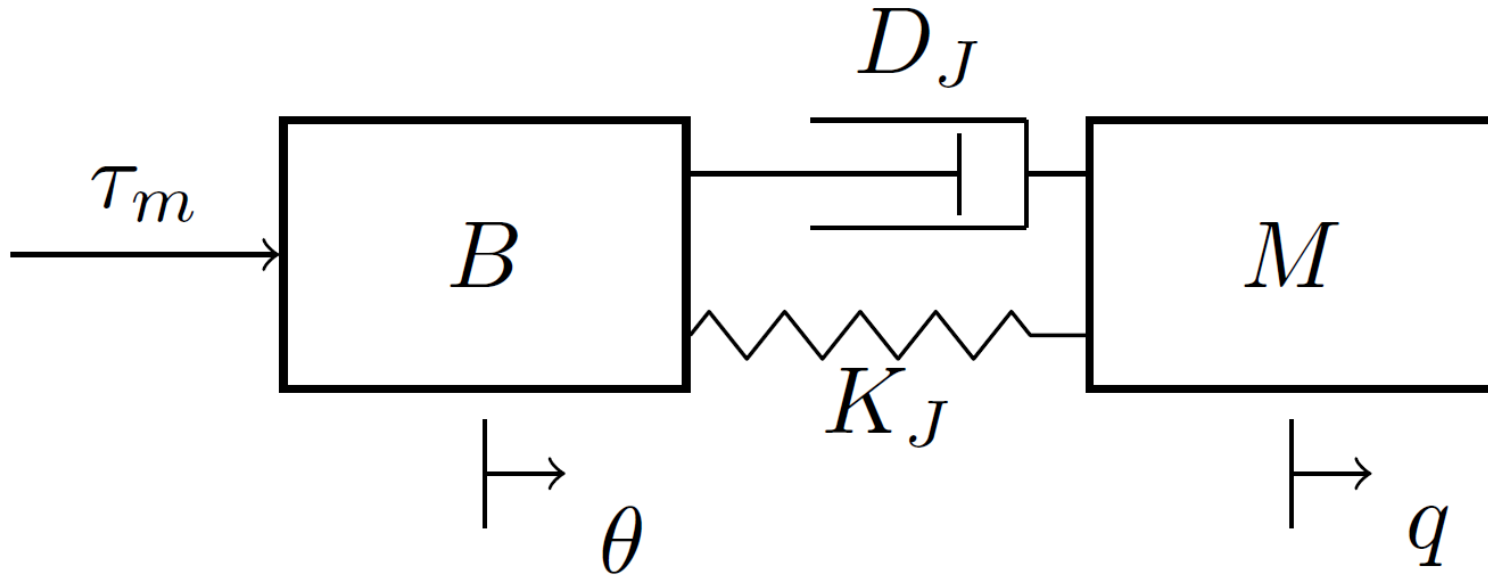


Variety of Problems

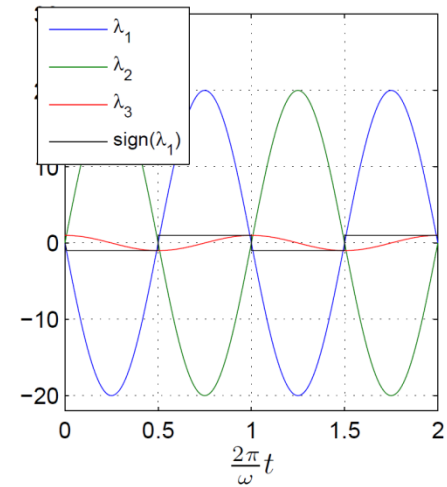
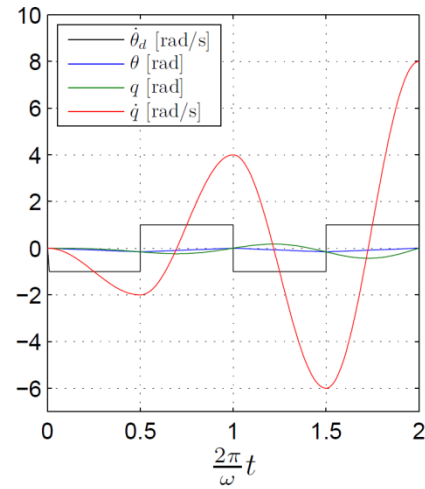
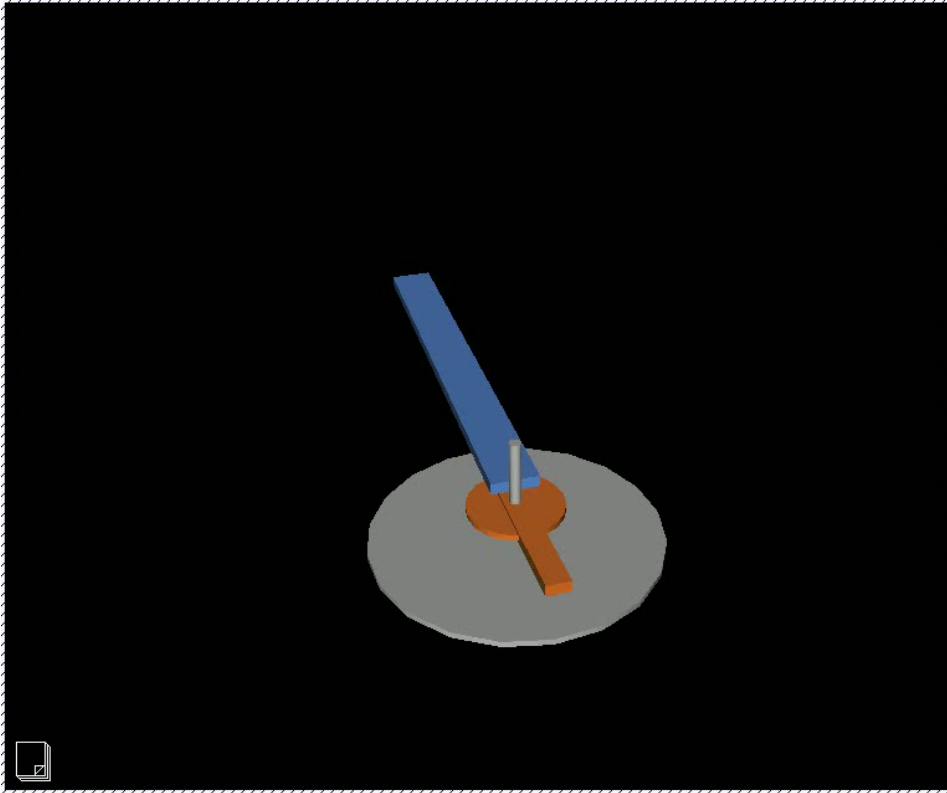
1-DoF Systems		N-DoF Systems	
SEA	VSA	SEA	
Velocity Input $\dot{\theta} \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ Unconstrained System Sec.III.A Limited Deflection ϕ Sec.III.F	Velocity and Stiffness Inputs $\dot{\theta} \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ $k \in [k_{min}, k_{max}]$ Unconstrained System Sec.IV		
Acceleration Input $\ddot{\theta} \in [\ddot{\theta}_{min}, \ddot{\theta}_{max}]$ Unconstrained System Sec.III.B Limited Motor Vel. $\dot{\theta}$ Sec.III.E	Velocity and Stiffness Inputs $\dot{\theta} \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ $k \in [k_{min}, k_{max}]$ Unconstrained Double Pendulum Sec.V.A Full Dynamics Sec.V.B.3	Velocity Inputs $\dot{\theta} \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ Unconstrained Double Pendulum Sec.V.A Linearized Dynamics Sec.V.B.1 Full Dynamics Sec.V.B.2	
Torque Input $\tau_m \in [\tau_{min}, \tau_{max}]$ Unconstrained System Sec.III.C Limited Motor Vel. $\dot{\theta}$ Sec.III.E	Velocity and Stiffness Motor Inputs $\dot{\theta} \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ $k = k(\sigma)$ DLR Hand-Arm System with Real-World Constrains Sec.V.C.1 Experiments: SEA, VSA Sec.V.C.2 Simulations: SEA, VSA Sec.V.C.2		
Controller Input $\dot{\theta}_d \in [\dot{\theta}_{min}, \dot{\theta}_{max}]$ QA-Joint with Real-World Constraints Sec.III.G Motor Models PT_1, PT_2 Appx. A			



1DoF Case



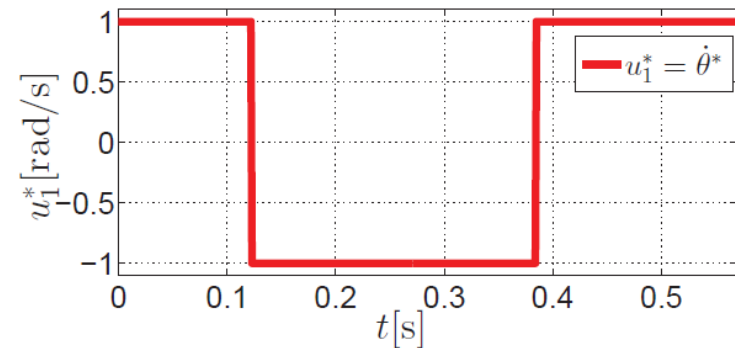
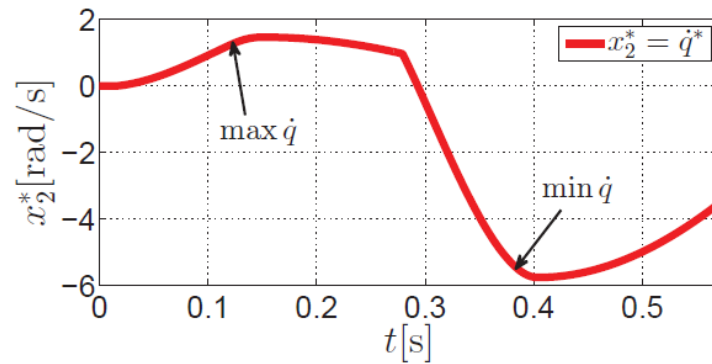
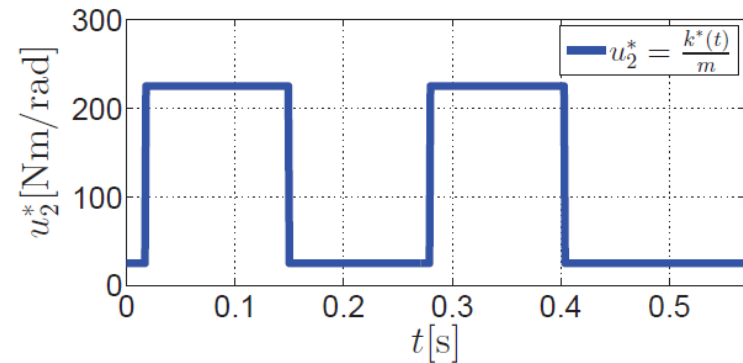
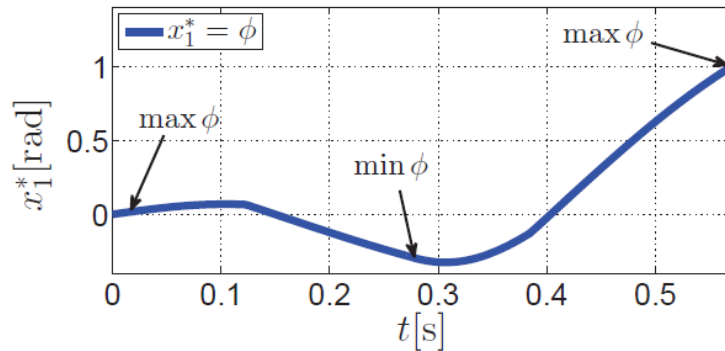
Simple 1DoF case



$$\dot{\theta}_d^* = \dot{\theta}_{\max} \operatorname{sgn}(\sin(\omega(t - t_f)))$$

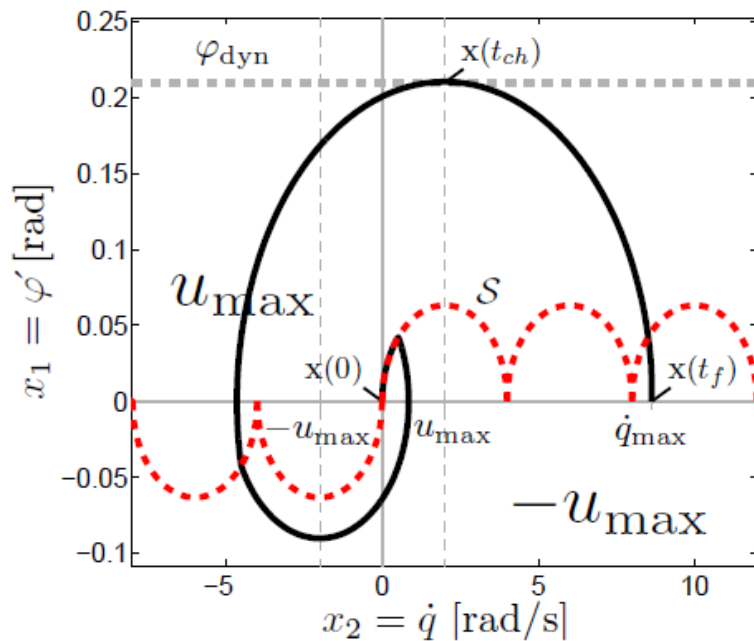


Example 1: $u_1 = \dot{\theta}, u_2 = k(t)$

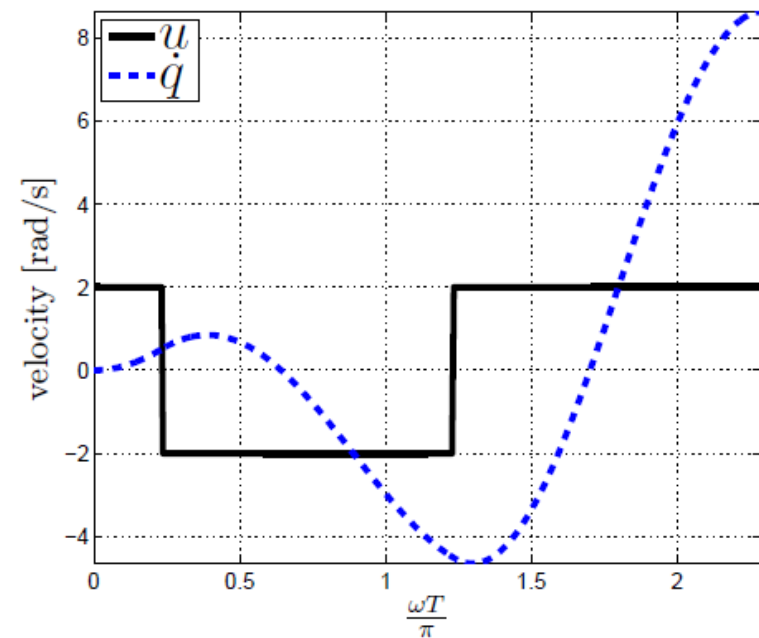


Example 2 (high spring energy): $u_1 = \dot{\theta}, \varphi \leq \varphi_{max}$

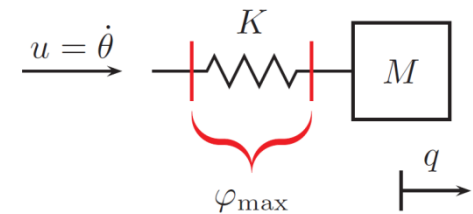
Phase plot:



Motor and link velocity:

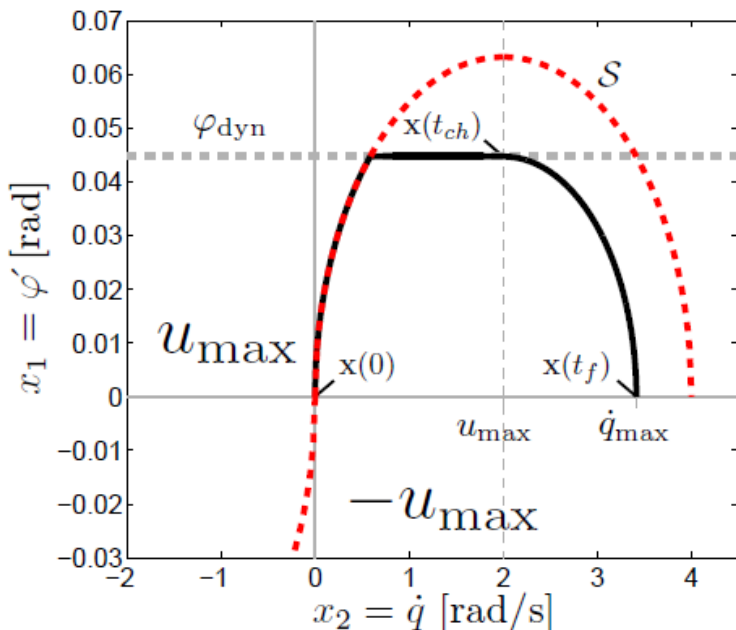


- Eigenfrequency excitation \rightarrow multiple bang-bang cycles

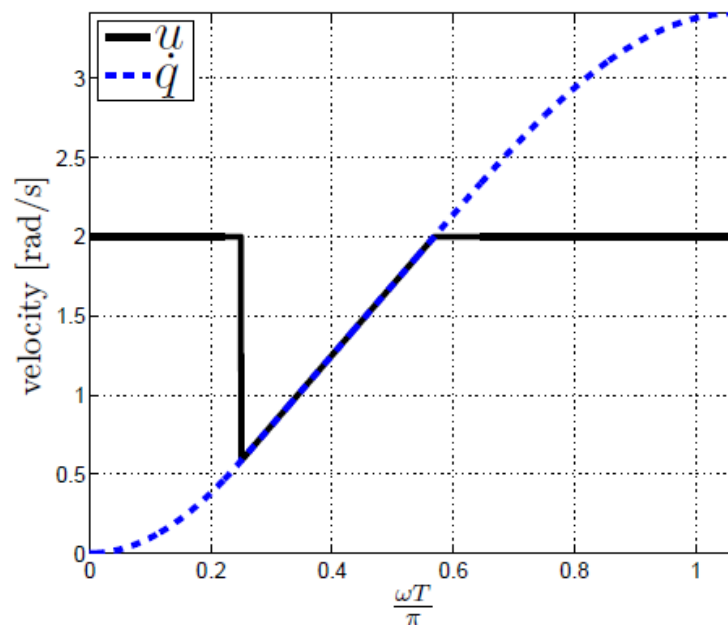


Example 2 (low spring energy): $u_1 = \dot{\theta}, \varphi \leq \varphi_{max}$

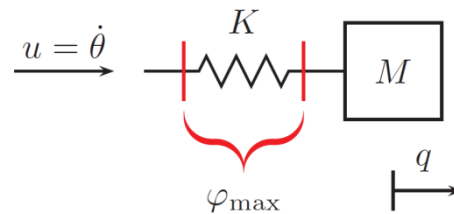
Phase plot:



Motor and link velocity:



- Singular arc: max. deflection used for link acceleration



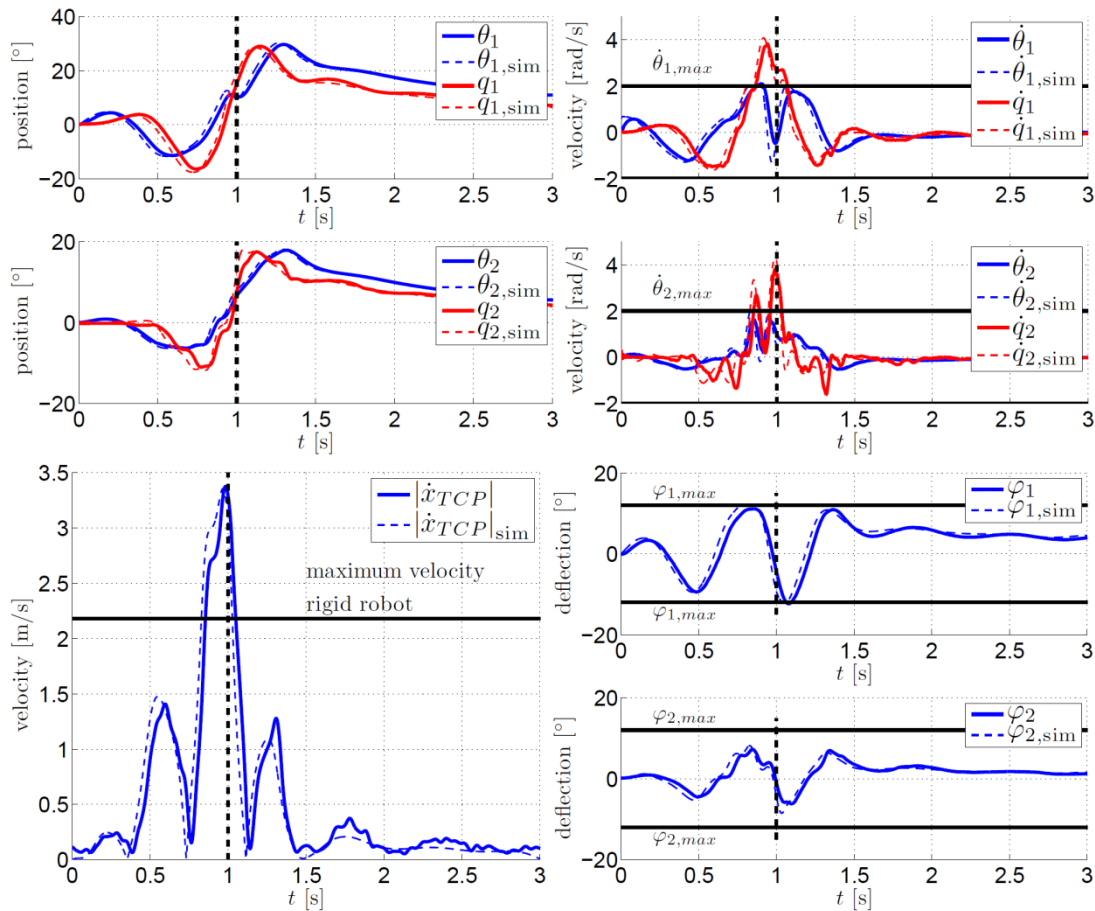
Full arm



Full arm



Experimental Data



Inherent Problem & Approach

Optimal control problems with full dynamics not analytically solvable

Robots are sought for dynamic environments and interaction, therefore, online is necessary!

$$M(\mathbf{q})\ddot{\mathbf{q}} + C(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \boldsymbol{\tau}_J$$

$$B\ddot{\Theta} + \boldsymbol{\tau}_J = \boldsymbol{\tau}_m$$

$$\boldsymbol{\tau}_J = \boldsymbol{\tau}_J(\Theta, \mathbf{q}, \boldsymbol{\sigma}),$$

Idea:

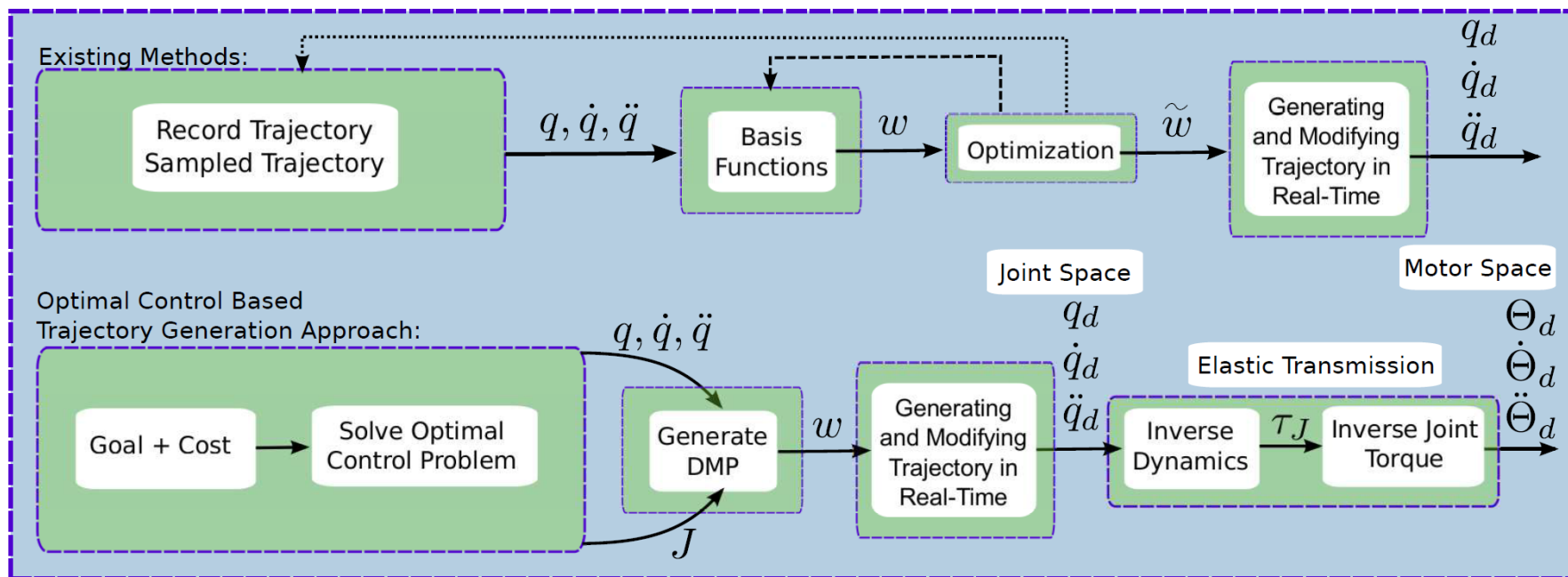
1. Learn **optimal** motions
2. Generalize with dynamical systems and a cost based neighborhood metric

Remark:

Decoupling property: Learn **joint torques** and ignore motor dynamics

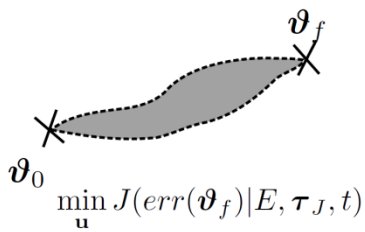


Optimal Learning and Generalisation Framework

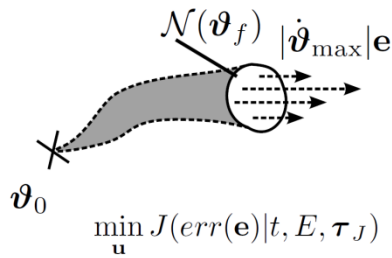


Prototypical OC Problems

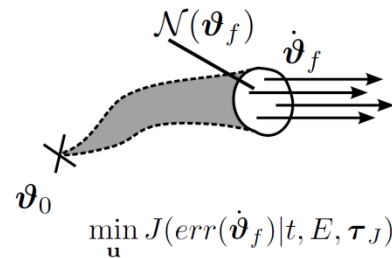
1.) reaching



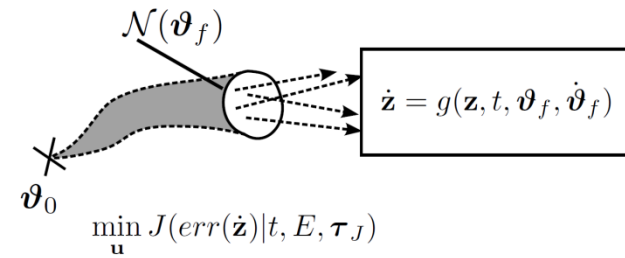
2.) explosive



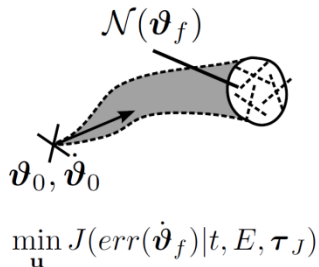
3.) explosive target



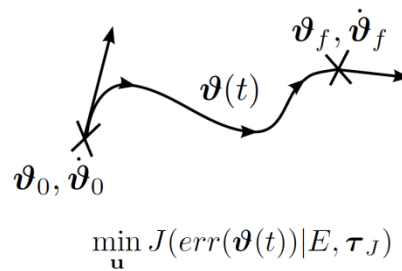
4.) implicit target



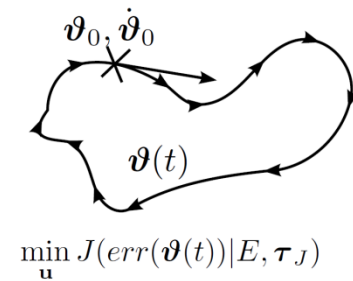
5.) implosive



6.) tracking



7.) cyclic tracking



Learning

input : motion type, $\mathbf{c}(\mathbf{q})$, parameters $\{\boldsymbol{\xi}_k\}$

output: \mathbf{w}^* , Φ^*

for $k \leftarrow 1$ **to** m **do**

$[\mathbf{q}_k^*, \dot{\mathbf{q}}_k^*, \ddot{\mathbf{q}}_k^*] = \min_{\mathbf{u}} J(\text{motion type}, \mathbf{c}(\mathbf{q}), \boldsymbol{\xi}_k) ;$

for $i \leftarrow 1$ **to** n **do**

$\mathbf{f}_i^*(t_i) = -\tau^2 \ddot{\mathbf{q}}^*(t_i) + \kappa(t_i)(\mathbf{q}^*(\tau) - \mathbf{q}^*(t_i)) - D\tau \dot{\mathbf{q}}^*(t_i) ;$

$x_i = \exp \left\{ -\frac{\alpha_x}{\tau} t_i \right\} ;$

$\mathbf{x}_i = [x_i; \dots; x_i]_{dim=M \times 1} ;$

$\mathbf{F}_k^* = [\mathbf{F}_k^*; \mathbf{f}_i^{*T}(t_i)] ;$

$\mathbf{X} = [\mathbf{X}; \mathbf{x}_i^T] ;$

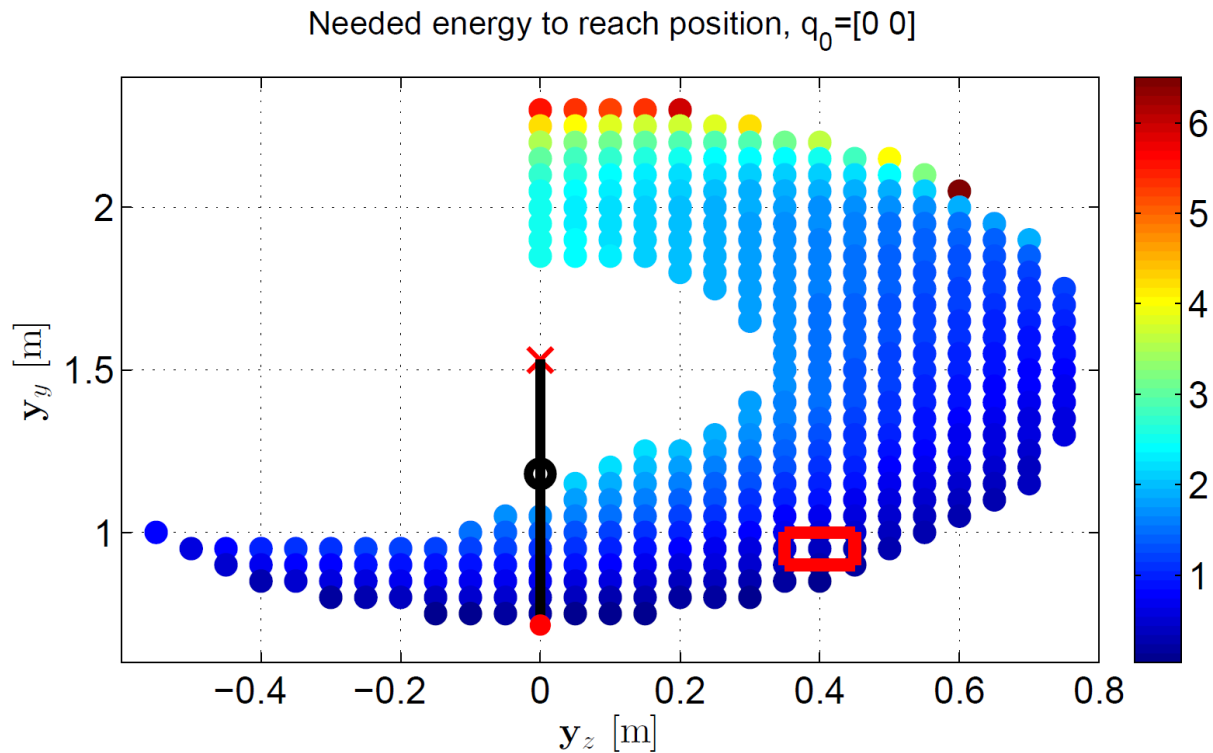
end

$[\mathbf{w}_k^*, \Phi^*] = \min \Gamma[(\Phi^j, \mathbf{F}_k^*, \mathbf{X}) \rightarrow \mathbf{w}^j \rightarrow \mathbf{f}_{\approx}^j]$

end



Example cost manifold



$$\min_{\dot{\Theta}(t)} J = \int_{t_0}^{t_f} \left(\frac{1}{2} w_{\Theta_1} \dot{\Theta}_1^2 + \frac{1}{2} w_{\Theta_4} \dot{\Theta}_4^2 \right) dt$$



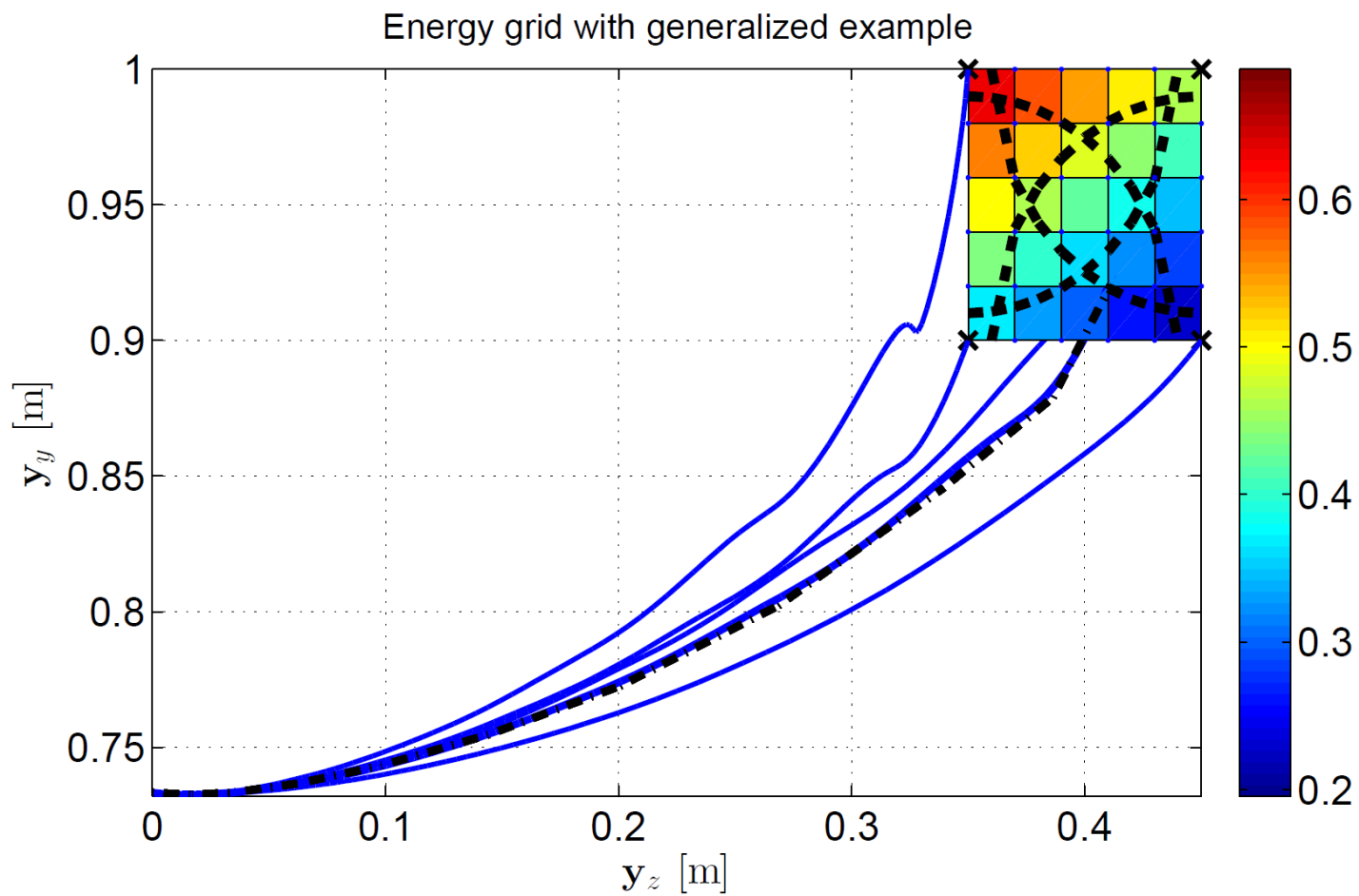
Generalization

$$\mathbf{w}_l^*(\mathbf{y}_g) = \frac{\sum_{\forall k: \sigma_k \leq \delta} \mathbf{w}_l^*(\mathbf{y}_k) \sigma_k^{-1}}{\sum_{\forall k: \sigma_k \leq \delta} \sigma_k^{-1}}$$

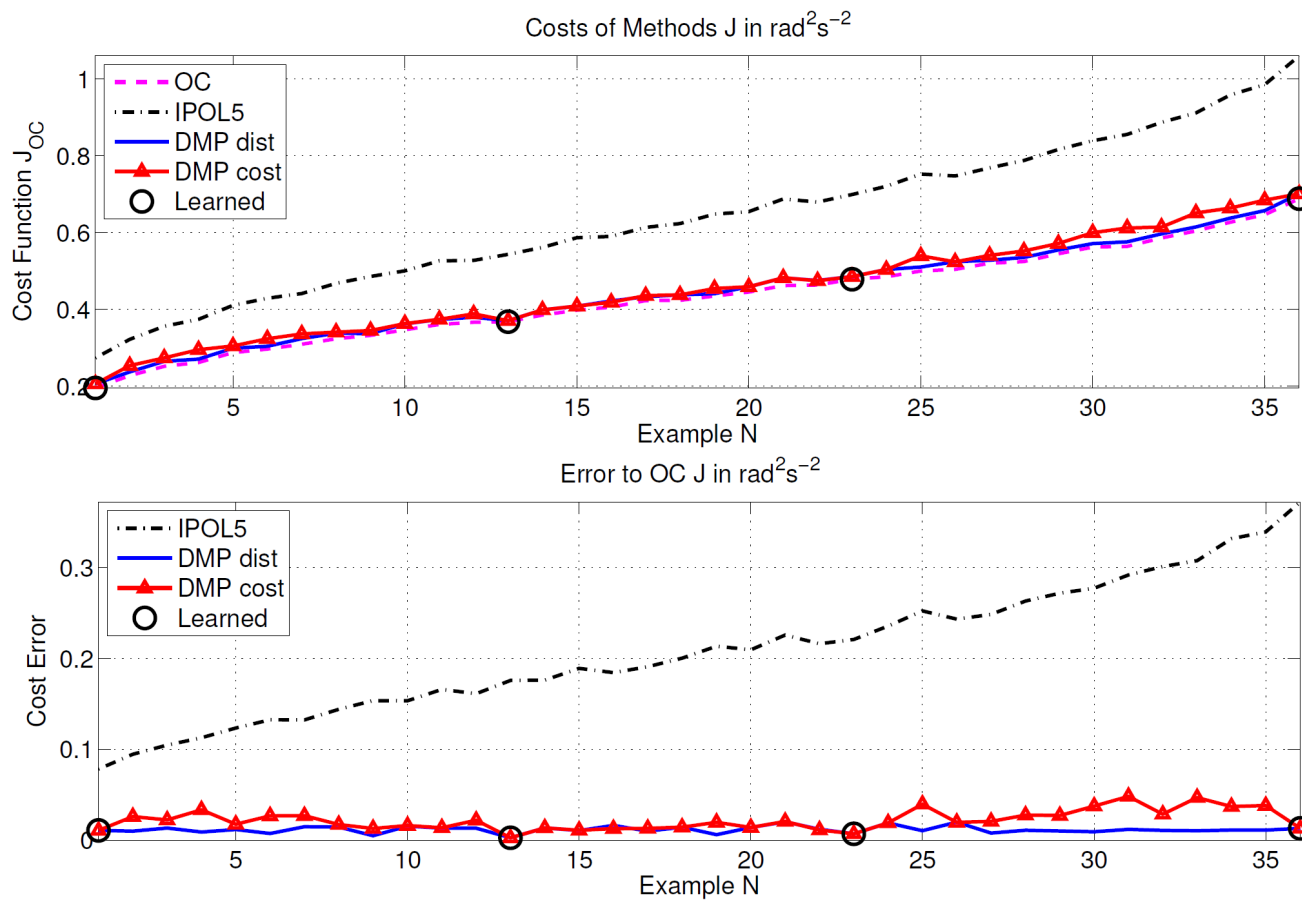
$$\sigma_k = \begin{cases} \|\mathbf{y}_g - \mathbf{y}_k\| + \epsilon, & \|\mathbf{y}_g - \mathbf{y}_k\| + \epsilon < \delta \\ \epsilon, & \|\mathbf{y}_g - \mathbf{y}_k\| + \epsilon \geq \delta \end{cases}$$



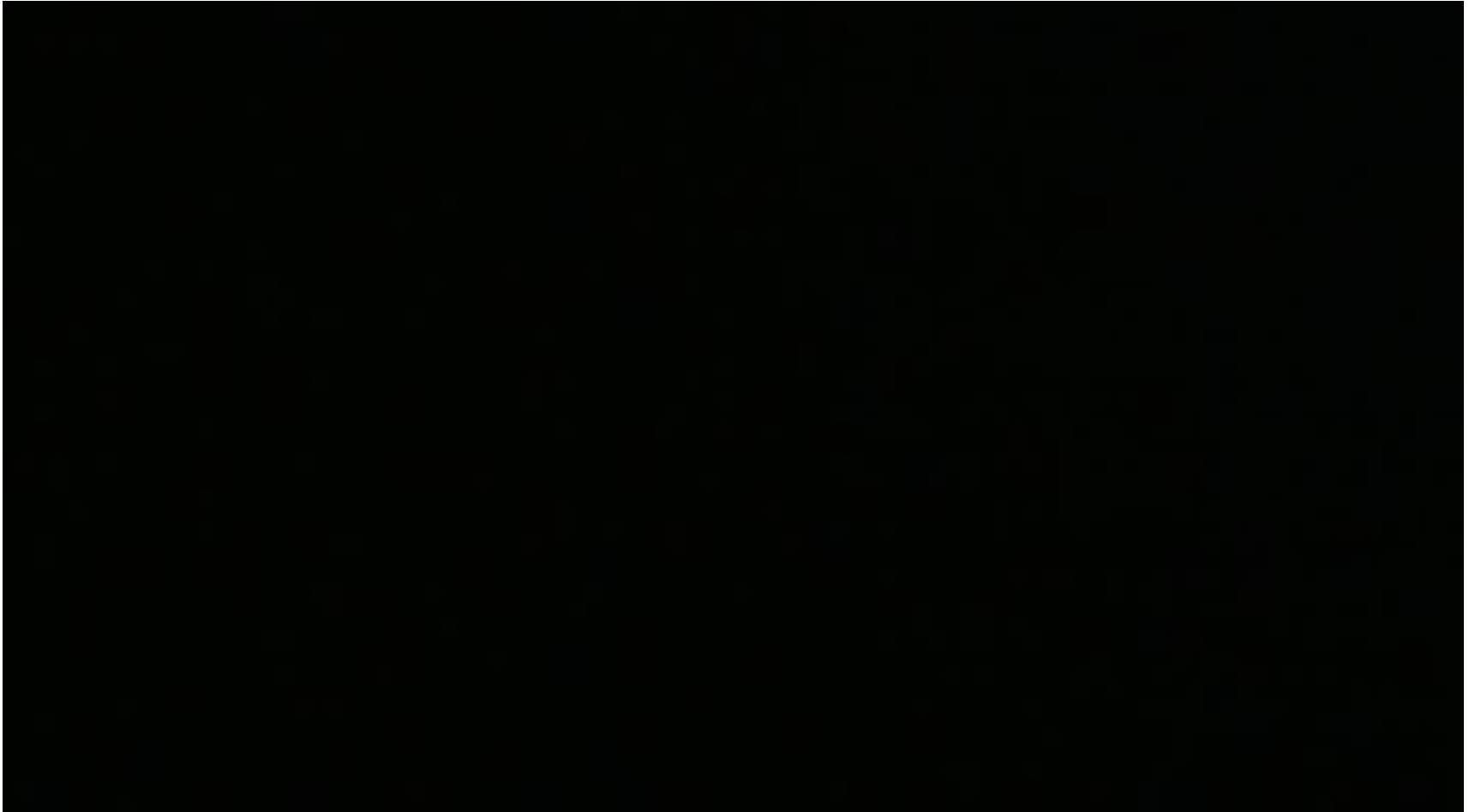
Generalization



Example: Point-2-Point Motion



Intrinsic Elasticity



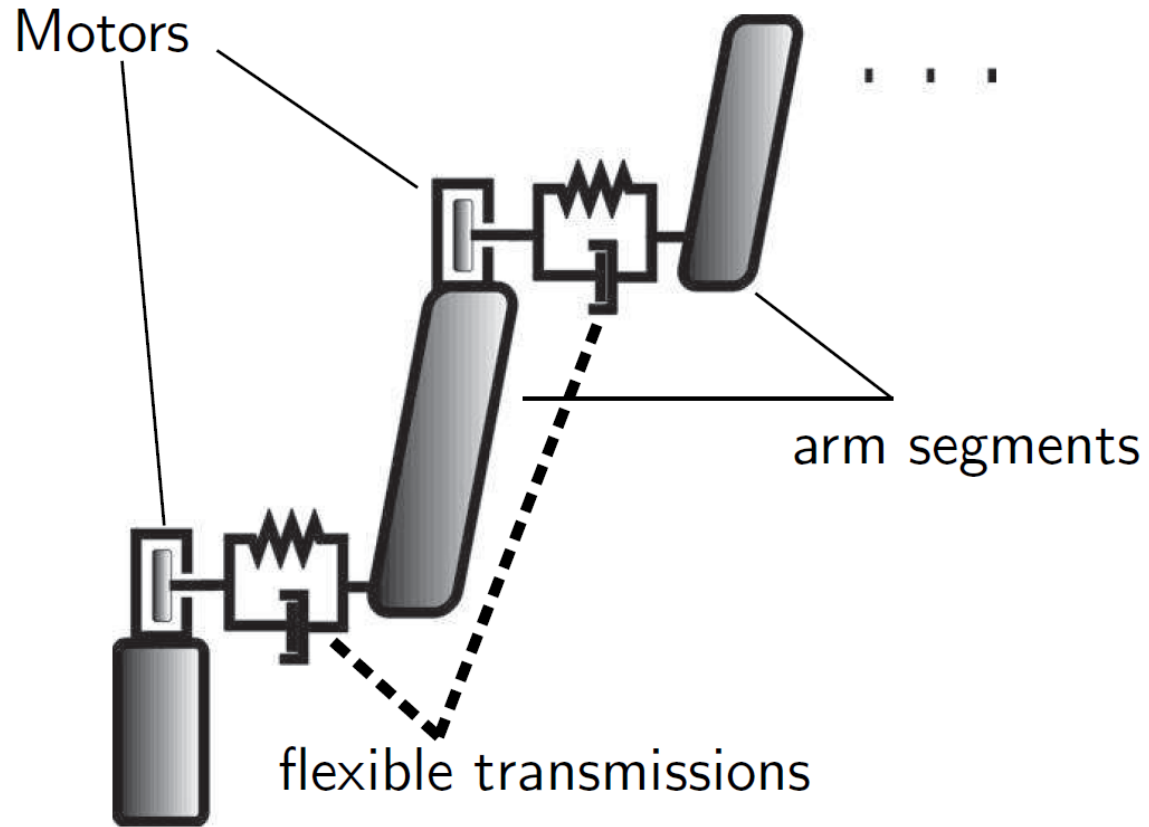
Thanks!



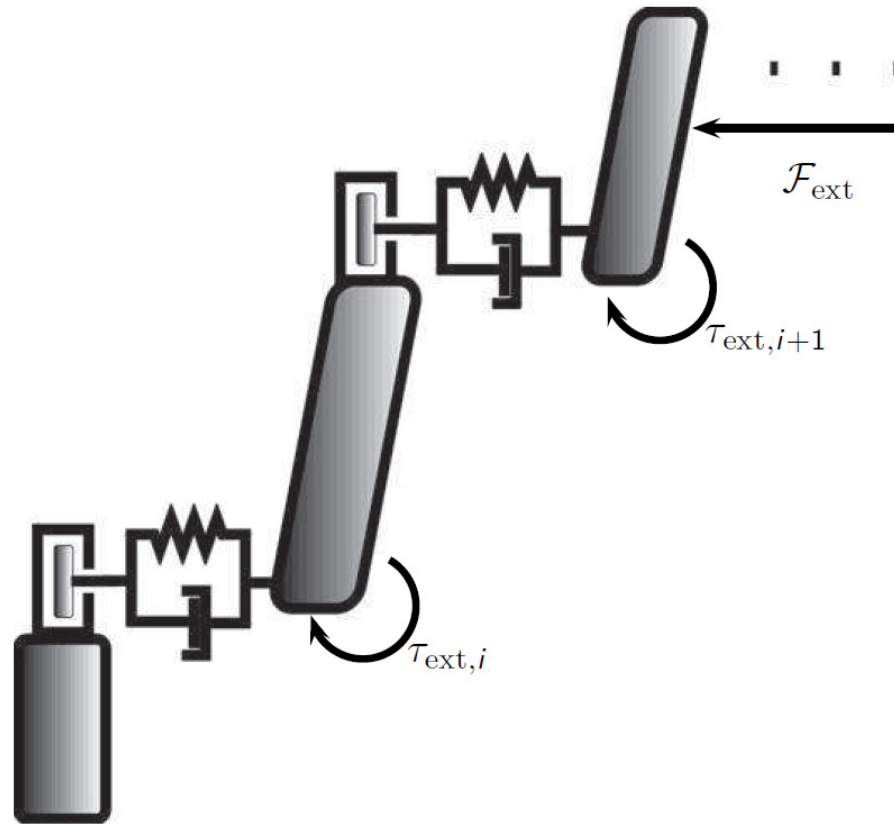
Collision detection & reflex reaction



Flexible Robots



Flexible Robots

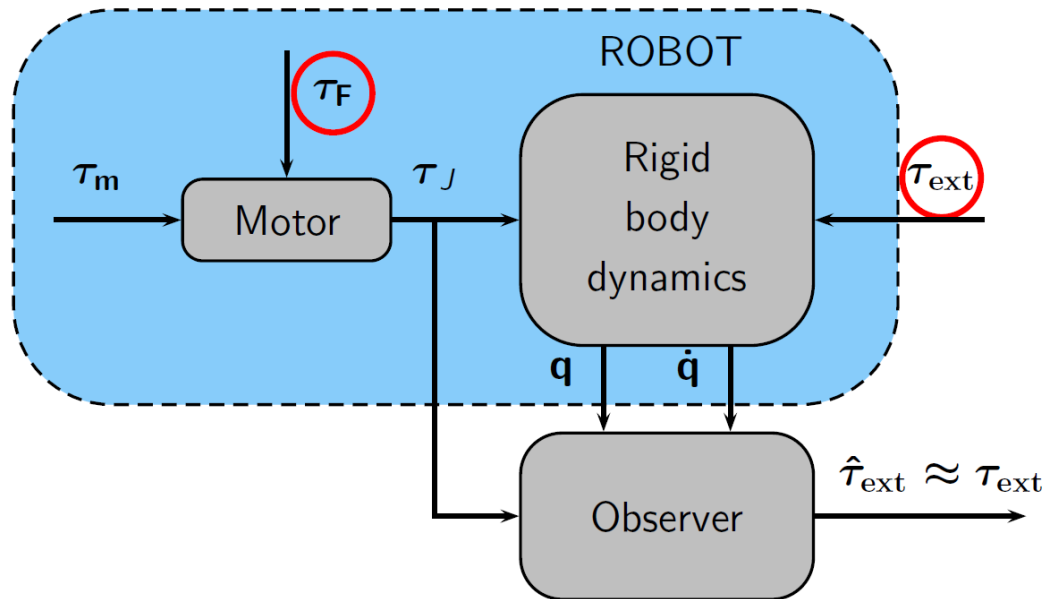


Collision Detection and Estimation

Flexible Joint Dynamics:

$$M(\mathbf{q})\ddot{\mathbf{q}} + C(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{g}(\mathbf{q}) = \boldsymbol{\tau}_J + \boldsymbol{\tau}_{\text{ext}}$$

$$B\ddot{\boldsymbol{\theta}} + \boldsymbol{\tau}_J = \boldsymbol{\tau}_m$$



Observer Design

Idea: Observe generalized momentum

$$\mathbf{p} = M(\mathbf{q})\dot{\mathbf{q}}$$

Reformulated dynamics:

$$\dot{\mathbf{p}} = \boldsymbol{\tau}_J - \boldsymbol{\beta}(\mathbf{q}, \dot{\mathbf{q}}) - \boldsymbol{\tau}_{\text{ext}}$$

Residual model:

$$\hat{\mathbf{r}} = \hat{\boldsymbol{\tau}}_{\text{ext}} \quad \dot{\hat{\mathbf{r}}} = \mathbf{0}$$

Observer design:

$$\hat{\mathbf{r}} = K_O \left(\int_0^T [\boldsymbol{\tau}_J - \boldsymbol{\beta}(\mathbf{q}, \dot{\mathbf{q}}) - \hat{\mathbf{r}}] dt - M(\mathbf{q})\dot{\mathbf{q}} \right)$$



Decoupled Estimation of External Torques

$$\hat{r}^i = \frac{1}{sT_O^i + 1} \tau_{\text{ext}}^i = \frac{K_O^i}{s + K_O^i} \tau_{\text{ext}}^i \approx \tau_{\text{ext}}^i \quad \forall i \in \{1, \dots, n\}$$

